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Construction Completion and Construction Quality Assurance Report

Gibbons Creek Environmental Redevelopment Group Gibbons Creek Steam Electric Station Site F Landfill Closure Cap 12824 FM 244, Anderson, TX 77830 June 6, 2025

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1.0 INTRODUCTION

1.1 GENERAL

On behalf of the Gibbons Creek Environmental Redevelopment Group (GCERG), HDR Engineering, Inc. (HDR) has prepared this report detailing the construction and quality (CQA) assurance activities associated with the construction of the Site F Landfill's (SFL) composite landfill cap at the Gibbons Creek Steam Electric Station (GCSES) in Grimes County, Texas. The landfill cap was constructed in accordance with 40 CFR §257.102(d) and 30 TAC §352.1221 for managing coal combustion residual (CCR) waste.

The SFL was originally designed and operated to manage waste which consisted primarily of fly ash, bottom ash, and stabilized FGD sludge. The waste deposited at the Landfill was considered as a Class II and Class III Industrial Non-Hazardous Waste (waste) by the Texas Water Commission (TWC)¹ in 1990.

The landfill was constructed by the Texas Municipal Power Agency (TMPA) in 1990 and expanded in 1995 to increase the onsite disposal capacity for the wastes generated by the GCSES. Since the SFL was constructed and received wastes meeting the criteria as coal combustion residuals (CCRs) as defined by 40 CFR §257.53, the landfill is considered an existing CCR landfill. In addition, the SFL is listed as a solid waste management unit, SWMU 001, on the notice of registration (NOR) for SWR 32271 issued to TMPA by the TCEQ. The NOR currently states that the SFL is an active SWMU.

No records of the actual SFL liner construction were available for review for inclusion in this report. However, according to TMPA's 1988 request for proposal to engineer and design the Landfill, this Landfill was to have a base liner system constructed with clay-rich soil placed and compacted in lifts with a total thickness of 3-feet. The liner was to be constructed using soils with the following characteristics:

- A unified soil classification of SC, CL, CH, or MH
- A percent passing No. 200 sieve greater than 30
- A liquid limit greater than 30
- A plastic index greater than 15
- A hydraulic conductivity no greater than 1 x 10⁻⁷ cm/sec.

A clay barrier was installed on the uppermost tier and portions of the first and second tier representing approximately 40-acres of intermediate cover for the SFL in approximately 1995. This clay barrier was comprised of soils meeting the same characteristics and thickness as the

¹ The Texas Water Commission (TWC) was combined with the Texas Air Control Board to become the Texas Natural Resource Conservation Commission (TNRCC) in 1993. In 2002, the TNRCC became the Texas Commission of Environmental Quality (TCEQ).

landfill's compacted clay bottom liner system. The barrier was covered in approximately 2-feet of topsoil and general fill designed to limit erosion and promote vegetative growth.

The purpose of this project was to permanently close the SFL by installing a final landfill cap meeting the requirements of 40 CFR §257.102(d)(3) and 30 TAC §352.1221 for managing coal combustion residual (CCR) waste. The area of the SFL final cover is approximately 95-acres and, according to GCERG personnel, the volume of CCR disposed on-site is estimated to be 8,224,601 cubic yards.

This report is accompanied by as-built drawings, daily field observation reports, and test results which document the construction oversight and construction quality assurance (CQA) work performed on the SFL's final landfill cap construction. HDR was retained to complete the SFL cap construction design, perform the CQA oversight during construction activities, and prepare this comprehensive report at the conclusion of the project.

The landfill cap construction work at the SFL liner is in accordance with the design and requirements contained in the following documents (see Appendix D):

- Gibbons Creek Electric Station Site F Landfill Closure construction drawings issued on August 2, 2021.
- Gibbons Creek Environmental Redevelopment Group, LLC Site A and Site F Landfill Closure Construction Documents Project Manual issued on August 2, 2021, which contained the project's technical specifications.
- Gibbons Creek Steam Electric Station Site A and Site F Landfill Closure Final Cover Quality Control Plan issued on August 2, 2021, which contained the project's quality assurance requirements.

As evidenced by the project documentation and testing program results, the landfill cap construction activities performed on the SFL were performed in accordance with the construction drawings, technical specifications, and CQA program.

1.2 PROJECT SUMMARY

The GCSES is owned by GCERG and is located near Anderson, Texas. The Site F Landfill (SFL) is approximately 95-acres in size and was designed and operated to manage Class II and Class III industrial non-hazardous waste which consisted primarily of CCR material such as fly ash, bottom ash, and stabilized FGD sludge. This material was generated through the combustion of local lignite to produce power at the GCSES. The SFL is located approximately 1.5-mile northeast of the administration buildings at the GCSES as shown in Figure 1 below.



Figure 1: Site F Landfill Location



Figure 2: Site F Landfill circa 2019

HDR served as the design and CQA engineer for the project. HDR's CQA Team was comprised of HDR and JBS staff which provided construction oversight and CQA services during construction. Construction progress was documented and photographed in daily field reports (DFRs) based on daily observations. The DFRs can be found in Appendix C: Landfill Cap Construction Quality Assurance Documents.

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17111 Preston Road, Suite 300, Dallas, TX 75248-1232 (972) 960-4400 At the portions of the landfill with an existing clay barrier and topsoil installed, this project generally consisted of removing the existing vegetation and topsoil over the existing compacted clay barrier. The uppermost 12-inches of the existing clay barrier was reprocessed, rehydrated, recompacted, and smooth rolled to establish a stable subgrade for the placement of the geomembrane.

At uncovered portions of the landfill, the waste material was compacted, graded, and smooth rolled. A 12-inch layer of general fill material was placed on top of the waste material to establish a stable subgrade for the landfill cap. A 12-inch layer of compacted clay meeting the characteristics of the landfill's liner system was installed over the stable subgrade.

On both portions of the landfill, after the compacted clay portion of the cap was completed, a new 40-mil linear low-density polyethylene (LLDPE) liner was placed over the surface of the smooth clay subgrade. The geomembrane was topped with a geocomposite geotextile. An 18-inch-thick layer of soil fill material and 6-inch-thick layer of topsoil were then installed over the geosynthetics. Stormwater controls were then constructed on the SFL and vegetative cover was re-established.

The landfill cap construction consisted of the list of activities presented below:

- Vegetation and topsoil were stripped and removed from the SFL and stockpiled.
- The upper 12-inch-thick layer of the existing compacted clay barrier was ripped, reprocessed, rehydrated, disced, recompacted, and regraded.
- Waste material at uncovered portions of the landfill were graded, compacted, and smooth rolled.
- A 12-inch-thick layer of soil was placed on top of the exposed waste material.
- A 12-inch-thick layer of compacted clay soil was placed on top of the subgrade.
- The compacted clay was rolled to establish a smooth stable base for the geosynthetics.
- A new 40-mil linear low-density polyethylene (LLDPE) liner was placed over the compacted clay layer.
- A geocomposite was placed over the geomembrane to promote drainage and stability for the landfill cap.
- An 18-inch-thick layer of soil was placed over the geosynthetics.
- A 6-inch-thick layer of topsoil was placed on top of the protective soil layer.
- The landfill was graded to promote stormwater drainage which included a series of ditches, swales, and berms installed to contain and direct stormwater.
- Concrete structures were installed to convey stormwater from the upper levels of the landfill to perimeter discharge culverts.
- Vegetation was established over the landfill.

1.3 Key Personnel

A list of the key organizations that participated in relining the SFL, along with their respective roles and key personnel, is presented below:

<u>OWNER</u> Gibbons Creek Environmental Redevelopment Group, LLC

DESIGN AND CQA ENGINEER HDR Engineering, Inc.; Dallas, TX Design Engineer and CQA Officer – David Vogt, P.E. (Texas 93905) CQA Monitor – Montreal Bailey JBS Engineering and Environmental, Inc.; Bryan, TX CQA Monitor – Phil Cadarette

<u>RECORD SURVEYOR</u> Lacy Surveying, Inc.; Arp, TX Daniel Cooper, R.P.L.S.

<u>SITE GENERAL CONTRACTORS</u> Mine Services, Inc. (MSI); Rockdale, TX Project Principal – Eddie Noak Project Director – Vernon Lang Site Superintendent – Manny Lopez

B&C Services, Inc.; Caldwell, TX Project Principal – Chris McDaniel Site Superintendent – Luis Godinez

Burnside Infrastructure, LLC; Hearne, TX Project Principal – Jake Burnside Project Director – Alfred Acuna Site Superintendent – Micheal Ambriz

SPJD Ranch, LLC; Iola, TX Project Principal – James Dixon Site Superintendent – Joe Bill Derden

<u>GEOSYNTHETICS INSTALLER</u> EnviroCon Systems, Inc. (ECSI); Cedar Hill, TX Project Manager – Larry Munger Site Superintendent – Montana Site Superintendent – May

<u>GEOSYNTHETICS MATERIALS TESTING LABORATORY</u> TRI Environmental; Austin, TX Laboratory Manager – Mansukh Patel

<u>GEOMEMBRANE, GEOCOMPOSITE, AND GEOSYNTHETIC CLAY LINER MANUFACTURER</u> Solmax Geosynthetics, LLC.; Houston, TX

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2.0 LANDFILL CAP CONSTRUCTION PREPARATION

2.1 Vegetation and Topsoil Removal

The contractor cleared and grubbed existing vegetation on top of the SFL. A dozer was used to strip the vegetation and top layer of soil off the landfill. This stripped material was removed using a front-end loader and placed in haul trucks. The stripped material was temporarily stockpiled at various locations around the SFL until it could be used as topsoil for the modified landfill cap.

2.2 Demolition of Existing Structures

The contractor used a track excavator and haul trucks to excavate and demolish the existing culverts, pipes, and concrete structures used to convey stormwater at the SFL. The excavator broke these items into smaller manageable pieces and loaded them onto a haul truck. The demolished material was hauled to the active area of the SFL where it was permanently disposed.

2.3 Placement of Waste Material and Fine Grading

The contractor used a dozer to place waste material at its final location in the active area of the SFL. The dozer was also used to fine grade the material to its final elevations. A smooth drum roller was used to compact the material, and a water truck was used for dust control.

3.0 COMPACTED CLAY CONSTRUCTION

3.1 Existing Clay Layer

The contractor used a Caterpillar D6 dozer to remove the top 6-inch layer from the existing clay barrier. This material was stockpiled adjacent to the working area using an excavator and haul truck. A ripper attachment was used by the dozer to break up and scarify the top 6-inches of the remaining existing clay barrier at the landfill. A water truck was used to hydrate the clay, and a disc attachment was used by the dozer to help process the existing clay barrier soils. A sheep's foot compactor was used to compact the clay to the proper density.

An excavator was used to load the stockpiled clay material on to a haul truck. The haul truck carried the clay material and placed it at the working area. A dozer spread the clay material to a loose thickness of approximately 8-inches over the processed clay layer. A water truck was used to hydrate the loosely placed clay material, and a disc was used to blend it in with the underlying processed clay layer. A sheep's foot compactor was used to compact the 8-inch loose clay material its design 6-inch lift thickness and density.

3.2 Active Area

An excavator was used to excavate clay soil material from preapproved borrow areas and load it on to a haul truck. The haul truck carried the clay soil material and placed it on top of the graded and compacted waste material in the working area. A dozer spread the clay material to a loose thickness of approximately 8-inches over the waste material. A water truck was used to

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hydrate the loosely placed clay material and sheep's foot compactor was used to compact the 8inch loose clay material a 6-inch lift thickness. Additional clay soil material was placed on the first layer in 8-inch thick loose lifts compacted to 6-inch thick lifts until the total clay barrier thickness was 18-inch thick. A disc was used to blend the clay material between the first and second lift and the second and third lift to create a monolithic clay barrier. The surface was then smooth rolled and compacted using a CAT CS54B smooth drum roller.

Density tests were performed on the compacted clay barrier in the field and barrier samples were collected and tested to determine its hydraulic conductivity in the lab in accordance with the project construction documents and CQA plan. Areas that did not achieve passing density or hydraulic conductivity results were reworked (ripped and disced), rehydrated, regraded, and recompacted until passing results were achieved.

4.0 GEOSYNTHTEIC INSTALLATION PREPARATION

4.1 Subgrade

Prior to the placement of geosynthetic material, the surface of the exposed clay barrier was smooth rolled and compacted using a CAT CS54B smooth drum roller. A water truck was used to moisture condition the subgrade and for dust control.

ECSI's construction quality control (CQC) personnel and HDR's CQA Team inspected the subgrade each day prior to deployment of the geomembrane liner panels to verify that the surface was firm, unyielding, free of excessive moisture, as well as free of cracking, unevenness from rutting, voids, and rocks that could damage the liner.

5.0 GEOSYNTHETIC INSTALLATION

5.1 Geomembrane Characteristics

The 40-mil LLDPE Textured Geomembrane manufactured by Solmax, LLC (Solmax) was used to line the surface of the SFL. This liner is a co-extruded textured linear low-density polyethylene (LLDPE) geomembrane.

Solmax provided manufacturer quality control (MQC) tests for the geomembrane to verify conformance with the technical specifications. The MQC test reports for the LLDPE geomembrane are included in Appendix B: Manufacturer Quality Control Certificates and summarized in Table 1: Geomembrane Manufacturer's Quality Control Test Summary. The test results indicated the LLDPE geomembrane rolls were manufactured in conformance with the project specifications.

The following tests are based on 3,813,887 ft² of 40-mil textured LLDPE geomembrane installed on the surface of the SFL. HDR reviewed the Manufacturer's Quality Control Test results and determined and confirmed the geomembrane was in conformance with project specifications.

		Frequency of	Minimum	Actual	Passing
Test	Type of Test	Testing	Required	Quantity	Quantity
	Thickness	Per Roll	267	267	267
	Density	Per 10 Rolls	27	27	27
	Carbon Black Content	Per 2 Rolls	134	134	134
Manufacturer's	Carbon Black Dispersion	Per 10 Rolls	27	27	27
Quality Control	Tensile Properties	Per 2 Rolls	134	134	134
	Tear	Per 5 Rolls	54	54	54
	Puncture	Per 5 Rolls	54	54	54
	Asperity Height	Per Roll	267	267	267

Table 1: Geomembrane Manufacturer's Quality Control Test Summary

The geomembrane rolls were manufactured from March 11 through March 30, 2022. Delivery of these rolls began on April 12, 2022, and continued through April 20, 2022. Each roll was assigned a unique number identifier by the manufacturer. Upon arrival at the site, HDR's CQA Team inspected the rolls for damage and verified the roll identifications met the shipping manifest. A Sky Trak forklift with a spreader bar attachment was used to offload the LLDPE geomembrane rolls from the delivery trucks. The Sky Trak then stockpiled the rolls on top of or adjacent to the SFL in areas designated by GCERG. The record of geomembrane received onsite is summarized on Appendix B: Landfill Cap Manufacturer Quality Control Certificates.

5.2 Geocomposite Characteristics

Solmax FabriNet Series 200 mil nonwoven calendared geocomposite was placed on top of the geomembrane to provide drainage and stability to the landfill cap. It has a 200-mil thick geonet core, and two 8 oz/yd² geotextiles.

5.3 Construction Quality Control and Construction Quality Assurance

Construction Quality Control (CQC) was provided by ECSI personnel on a full-time basis during the liner installation.

Construction Quality Assurance (CQA) monitoring of the installation and construction of the clay and geomembrane liner systems was performed on a full-time basis by one or more qualified engineering technicians under the direct supervision of the CQA Officer. CQA personnel observed and documented construction of the clay liner, proper soil material, proper thickness, and proper density as well as deployment of the geomembrane, proper overlap configuration, proper orientation of panels, all seaming operations and non-destructive testing of the geomembrane liner, measured seam lengths, recorded panel dimensions, located all patches and repairs, and monitored ambient temperature readings. Inspection reports and test results from the CQA effort are located in Appendix C: Landfill Cap Construction Quality Assurance Documents.

5.4 Geomembrane and Geocomposite Installation

Geomembrane liner panel deployment began along the uppermost tier of the landfill at the northeast corner. The panels were installed along the northern side of the uppermost tier of the landfill. In general, the panels were then installed southerly until the uppermost tier was complete. The panels were then installed on the interior slopes transitioning from the uppermost

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tier to the lowest tier. Panels were then installed over approximately 11 acres of the landfill its southern corner. Starting on March 30, 2023, panel installation at the SFL was paused while the site's remaining CCR material was transferred and placed at the SFL landfill. Geomembrane panel resumed on November 28, 2023, after the final waste material grading and compacted clay liner was installed, until the entire landfill was covered.

The Sky Trak with the spreader bar attachment was used to deploy each LLDPE geomembrane roll. A utility terrain vehicle (UTV) would use clamps to secure the geomembrane and then drive forward to deploy it across the surface of the landfill. Once the LLDPE geomembrane was deployed, ECSI personnel would manually adjust it to achieve a minimum overlap of 4-inches with an adjacent geomembrane panel. Loose panel ends were anchored by sandbags or unused rolls of geocomposite and all wrinkles and fish mouths were worked out or reduced. Each panel was assigned a unique number. The seam area was cleaned using rags and brushes to remove grease, moisture, dirt, and debris prior to seaming.

The Sky Trak with the spreader bar attachment was also used to deploy the geocomposite. A utility terrain vehicle (UTV) would use clamps to secure the geocomposite and then drive forward to deploy it across the geomembrane. Once the geocomposite was deployed, ECSI personnel would manually adjust it to achieve an approximate 2-inch overlap with an adjacent geocomposite panel. The adjacent geocomposite panels were then attached using zip ties and heat guns to fuse them together. Loose panel ends were anchored by sandbags or rolls of geocomposite.

No equipment was allowed on the geocomposite or geomembrane during deployment and seaming operations that could damage the liner system.

5.5 Geomembrane Seaming

Before the start of the day's seaming operations, each operator performed trial seams on their seaming equipment. These tests were also performed after the noon break and at other times deemed necessary by the CQA monitor. Each operator welded a minimum of 3-feet of geomembrane together for their trial seams and cut 6 sample coupons from this section for testing. Three of the coupons were tested in peel mode and three were tested in shear mode using a field tensiometer provided by ECSI. The minimum passing criteria is shown in Table 2: Minimum Required Seam Strength.

FAILURE MODE	TEST METHOD	VALUE(PPI)
Shear	ASTM D6392	60
Peel (fusion)	ASTM D6392	50
Peel (extrusion)	ASTM D6392	44

Table 2: Minimum Required Seam Strength

Only equipment that passed the trial seam test was permitted to be used to seam the geomembrane. Adjustments or repairs had to be made to equipment which failed the tests, until

it successfully passed the trial seam test. CQA test results documenting the trial seam, the welder, the welding apparatus number, time, date, ambient temperature, welding machine temperature, and speed are in Appendix C: Landfill Cap Construction Quality Assurance Documents.

The geomembrane seaming process occurred concurrently with the panel deployment. ECSI primarily used hot wedge double track fusion welders to seam the overlap where two sections of liner met. Extrusion welders were primarily used to seam patches at panel intersections (tees and cross joints) and HDPE pipe penetrations (pipe cleanout, piezometers, etc.). The patches were installed using the same material as the geomembrane. The seaming operations were observed and documented by HDR's CQA Team personnel and are summarized in Appendix C: Landfill Cap Construction Quality Assurance Documents.

5.6 Batten Strips

Batten strips were used to attach the geomembrane liner to the concrete stormwater down chutes. The batten strips were attached using stainless steel epoxied anchors installed into drilled holes spaced 6-inches apart along the concrete structures. A closed cell neoprene gasket was then affixed to the concrete using an adhesive. The edge of the geomembrane was placed on top of the neoprene gasket and a ¼-inch by 2-inch stainless steel flat bar was placed on top of the geomembrane. Stainless steel washers and nuts were then installed and tightened to form a waterproof seal for the geomembrane liner.

5.7 Geomembrane Repair

A repair patch was installed at each tee joint, cross joint, and defect observed during the geomembrane installation. A unique repair identification number was assigned to each of these repairs in accordance with the project specifications by HDR's CQA Team.

Small creases and holes smaller than ¼-inch in size were repaired by applying a bead of extrudate over the defect. Defects larger than ¼-inch in size were patched. The patches were oval in shape and extended a minimum of 6-inches beyond the intersection or defect. Defective seams, or seams that could not be nondestructively tested, were capped with a patch. Surfaces of the geomembrane receiving repair work were abraded and cleaned prior to the installation of the repair.

5.8 Non-Destructive Seam Continuity Testing

All double track fusion welded seams received an air pressure test. For this test, the air channel between the tracks of the two fusion welds were sealed off and an inflation needle and pressure gauge were inserted into the air channel. An air compressor then pressurized the channel to a minimum air pressure of 30 psi for a minimum of 5 minutes. A passing test was achieved if the seam held the pressure or lost no more than 3 psi during the time period. Following a passed pressure test, the seal on the opposite end of the seam was removed to allow release of the air. The pressure gauge had to return to zero to verify that there was no blockage(s) within the seam.

All patches, repairs or extrusion welds were vacuum tested utilizing a vacuum box. For this test, a soapy water solution was applied to the seam. A clear rigid wall box with a plastic plexiglass top

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and neoprene gasket around the bottom was placed over the seam and a vacuum of at least 3 psi was applied to the box creating a seal between the box and the geomembrane. A passing test occurred if no soap bubbles were observed during a ten second interval. A failing test occurred with the appearance of soap bubbles which were indicative of pinholes, porosity, or non-bonded areas in the repair.

If a seam failed non-destructive testing, then retesting would be performed to isolate the leak. The seam would then be repaired a minimum of 6-inches on either side of the leak and retested until all of the seam length passed. If the CQA monitor felt the seam was questionable during any phase of the geomembrane installation, then the seam would be destructively tested (refer to the Destructive Sample Test Results for details). The results of non-destructive tests performed indicated the seams were in conformance with the project specifications. Geomembrane Seaming Logs are located in Appendix C: Landfill Cap Construction Quality Assurance Documents.

5.9 Destructive Testing

The CQA personnel selected destructive test locations based on observations made during seaming or selected at random. There were 360 destructive tests performed on the geomembrane with 345 passing tests. For the non-passing destructive tests, two new destructive test samples were taken on the seam on opposite sides and 50 feet from the failed test location. These samples were tested and passed. A cap was then extrusion welded to the seam spanning the 100-feet distance between the two passing tests. All seams ultimately passed.

Each destructive sample measured 48 inches in length and 6 inches in width. This sample was divided into three sections approximately 16 inches in length. One section was tested in the field. The second was sent to TRI Environmental, Inc. for independent laboratory testing. The third section was kept for archival records.

Ten coupons were taken from each section for testing. Five coupons were tested for sheer strength and five coupons were tested for peel strength according to project specifications (see Table 2: Minimum Required Seam Strength). Each destructive test sample was considered to have passed when 4 out of 5 coupons met both the strength requirements and exhibited film tear bond (FTB). HDR confirmed that the results of all 766 passing destructive tests performed indicated the seams were in conformance with the project specifications. A summary of destructive sample results can be found in Appendix C: Landfill Cap Construction Quality Assurance Documents.

6.0 SOIL COVER

The geosynthetic components were covered with soil layers consisting of a 6-inch-thick layer of topsoil over an 18-inch-thick layer of soil fill material. A track excavator, articulated dump haulers, a dozer, smooth drum roller, and water truck were used to construct the soil layers on top of the geosynthetics. In general, the track excavator would excavate soil from the designated soil borrow area and place it in an articulated dump hauler. The articulated dump hauler would transfer the soil from the soil borrow area to the landfill. At the landfill the hauler would dump the soil into stockpiles adjacent to the exposed geosynthetics. The dozer was used to push and spread the soil piles onto the geosynthetics. After the

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desired soil layer thicknesses were achieved, the smooth drum roller would smooth out the surface of the soil and nominally compact it. Water trucks were used during the installation of the soil components to increase the soil moisture content and dust control.

The soils used for the landfill cap were generally classified as sandy or sandy clay free of rocks or other debris greater than 2-inch diameter. Ditches, swales, and berms were constructed as needed to convey stormwater off the landfill.

7.0 AS-BUILT SURVEY

Lacy Surveying, LLC (Lacy) was the record surveyor for this project. They performed survey operations throughout the project and their time on site is documented in the DFRs. Lacy provided as-built survey drawings of the Site F Landfill. Lacy completed the onsite surveying for the SFL reline project on December 11, 2024.

8.0 SUMMARY OF CONSTRUCTION MODIFICATIONS

The installation of the geosynthetics occurred in two phases. Phase 1 started on July 11, 2022, and ended on March 29, 2023. The work stoppage occurred because the Owner closed their Site A Landfill's (SAL) Perimeter Collection Ponds 2 and 3 and installed a new composite liner system in Ponds 1 and 4. All waste material and impacted soils from these ponds were excavated and hauled to the active area at the SFL for disposal by B&C Services. After the final waste material from the SAL was placed in the remaining open active area of the SFL, a topographical survey was performed, and the grading of the remaining open area was redesigned for final closure. Phase 2 of the geosynthetic liner installation started on November 28, 2023, and ended on February 15, 2024.

During Phase 1 of the geosynthetic installation at the SFL, MSI was the general contractor for the project and ECSI's liner installation team was managed by Montana. During Phase 2 of the geosynthetic installation, Burnside was the general contractor and ECSI used a new installation team managed by May. As evidenced by the project documentation and testing program results, the SFL closure cap was constructed in accordance with 40 CFR 257.102, 30 TAC §352.1221, CCR Closure Plan, and the August 2, 2021, project drawings, technical specifications, and QA/QC program.

HDR appreciates the opportunity to serve as your consultant on this Project and to submit this completion and CQA report for capping the SFL. If you have any questions concerning this report, please contact the undersigned.

David C. Vogt, PE

P.E. License #93905 Project Manager HDR Engineering, Inc. 17111 Preston Road, Suite 300 Dallas, TX 75248 Texas Engineering Firm No. 754

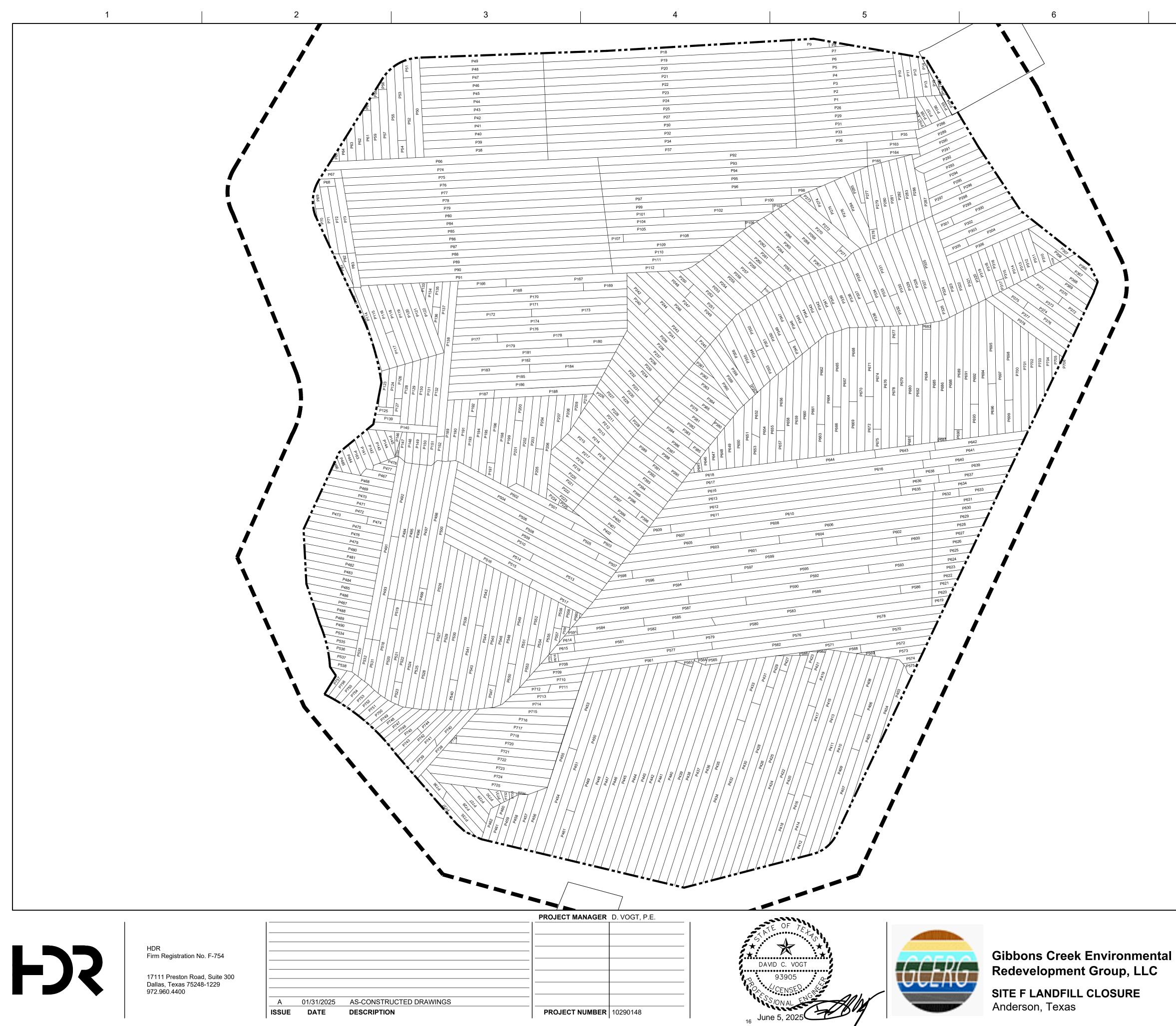


APPENDIX A

LANDFILL CAP AS-BUILT DRAWINGS

TOPOGRAPHIC SURVEY OF SITE F LANDFILL SURVEYED DECEMBER, 2024 AERIAL IMAGERY COLLECTED DECEMBER 11, 2024 SCALE: 1" = 200.00'





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GEOMEMBRANE PANEL LAYOUT AS-BUILT FILENAME SITE LAYOUT AS-BUILT.dwg GEOMEMBRANE PANEL AS-BUILT **SCALE** 1"=130'

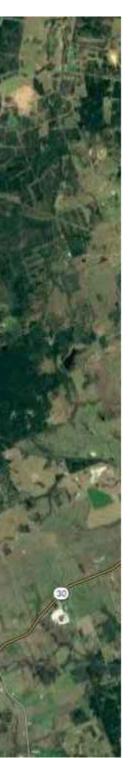


Gibbons Creek Environmental Redevelopment Group, LLC



VICINITY MAP





Construction Drawings For

Gibbons Creek Electric Station

Site F Landfill Closure

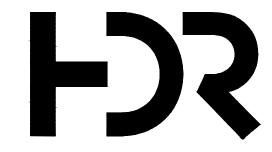
Project No. 10290148

Anderson, Texas June 2025



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HDR Firm Registration No. F-754 17111 Preston Road, Suite 300 Dallas, Texas 75248-1229 972.960.4400

INDEX OF DRAWINGS

GENERAL

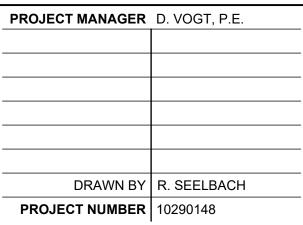
00G-01	COVER SHEET
00G-02	ABBREVIATIONS AND GENERAL NOTES
CIVIL	
00C-01	SURVEYOR GRID
00C-02	SITE PLAN
00C-03	ACTIVE AREA CCR PLACEMENT
00C-04	SUBGRADE PLAN - TOP OF COMPACTED CLAY LAYER
00C-05	INFILTRATION LAYER PLAN
00C-06	FINAL COVER PLAN
00C-07	CROSS SECTIONS
00C-08	DOWN CHUTE B & H
00C-09	BARNEY POND DOWN CHUTE
00C-10	DOWN CHUTE F
00C-11	MISCELLANEOUS DETAILS SHEET 1
00C-12	MISCELLANEOUS DETAILS SHEET 2

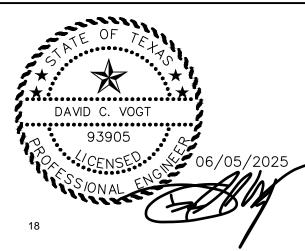
1		2	3	3
STANDAR) ABBREVIATIONS			
& APPROX @ AVG APS BOE BOL X CL CMP CO CY DIA DET DWG E ELEV EW EXIST EXC FGD FML FT GAL GCSES GCERG GND GDL GNDL HDPE HORIZ ID IN IE LCRS LCS LCP LCPR LF LB MH MAX MIL MIN MW MSL N NIC NO	AND APPROXIMATELY AT AVERAGE ASH PONDS BOTTOM OF EXCAVATION BOTTOM OF LINER BY CENTERLINE CORRUGATED METAL PIPE CLEAN OUT CUBIC YARD DIAMETER DETAIL DRAWING EAST ELEVATION EACH WAY EXISTING EXCAVATION FLUE GAS DESULFICATION FLUE GAS DESULFICATION FLEXIBLE MEMBRANE LINER FEET GALLON GIBBONS CREEK STEAM ELECTRIC GIBBONS CREEK STEAM ELECTRIC GIBBONS CREEK ENVIRONMENTAL GROUND GRAVEL DRAINAGE LAYER GEONET DRAINAGE LAYER HIGH DENSITY POLYETHYLENE HORIZONTAL INSIDE DIAMETER INVERT ELEVATION LEACHATE COLLECTION AND REM LEACHATE COLLECTION AND REM LEACHATE COLLECTION PIPE LEACHATE COLLECTION PIPE LEACHATE COLLECTION PIPE RISE INVERT ELEVATION LEACHATE COLLECTION PIPE RISE INVERT FLEET POUND MANHOLE MAXIMUM MONITOR WELL MEAN SEA LEVEL NORTH NOT IN CONTRACT NUMBER SYMBOLS CTION DETAIL INDICATORS WING ON WHICH SECTION APPEARS: NUMBER ON X-X X	STATION REDEVELOPMENT GROUP	NOI NTS OC OZ % PLCP PERF PGL PC PI PVI PT PZ Q Q QTY R RCP REF REQ RD SAL SCH SDL SEC SFL SHT S SDR SLQCP SP SSP SQ SS STA T.A.S. TL TOC TOFC TOL TOS TS TS TEMP TPDES TYP UNO VERT W W/ WW YD	NOTICE O NOT TO ON CENT OUNCE PERCENT PERFORA PERFORA PERFORA PROFILE POINT OF POINT OF SECTION SITE A L SCHEDUL SAND DF SECTION SITE F L SOUTH STEEL PI SCRUBBE SQUARE SIDE SLO STATION TERMINAI TANGENT TOP OF TOP OF
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	DE	TAIL IS INDICATED		
	ISSUED FOR CONSTRUCTION			
	HDR Firm Registration No. F-754			

17111 Preston Road, Suite 300 Dallas, Texas 75248-1229 972.960.4400

A 06/05/2025 AS-CONSTRUCTED DRAWINGS
ISSUE DATE DESCRIPTION

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PROJECT MA	ANAGER D. VOGT, P.E.		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		







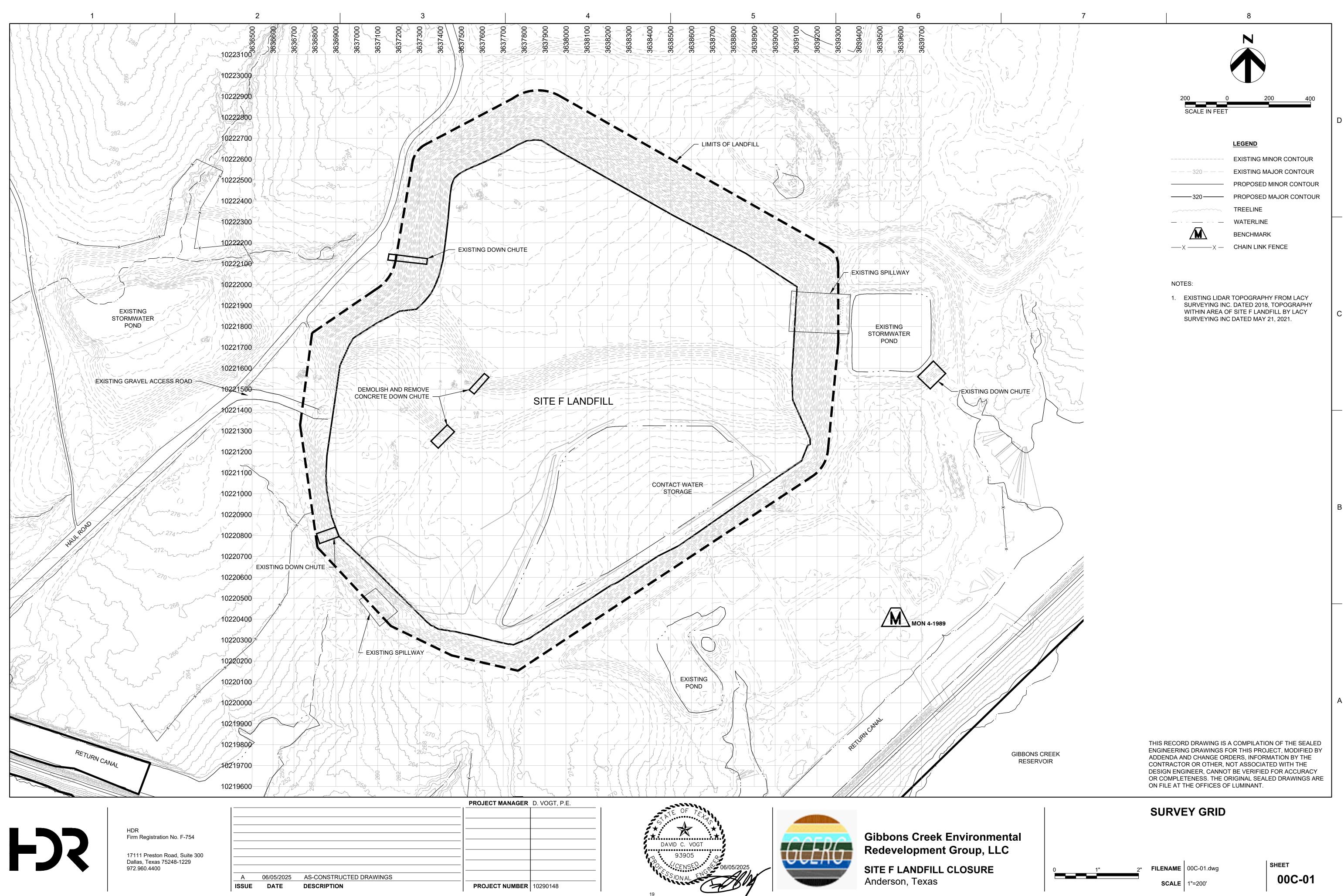
Gibbons Creek Environmental Redevelopment Group, LLC

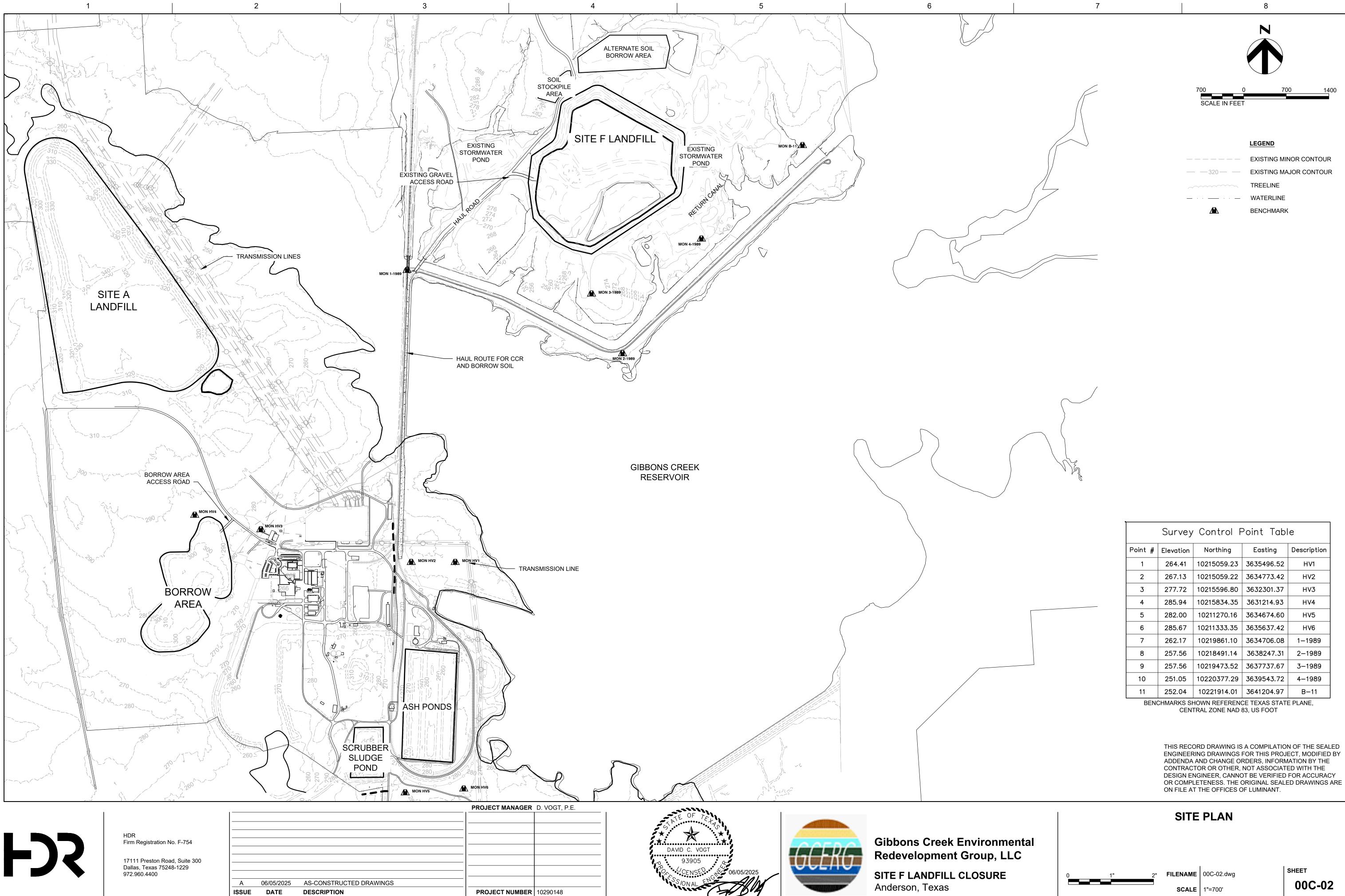
SITE "A" LANDFILL Anderson, Texas

GENERAL NOTES

CONTRACT SHALL BE PERFORMED IN ACCORDANCE WITH THE PLANS AND PROJECT SPECIFICATIONS. IN REPANCY BETWEEN THE PLANS AND THE PROJECT SPECIFICATIONS, THE SPECIFICATIONS SHALL GOVERN. IS BASED ON LOCAL SURVEY. THE BENCHMARKS TO BE USED FOR CONSTRUCTION ARE LOCATED AS SHOWN -01. EXISTING CONTOURS ARE BASED ON TOPOGRAPHICAL SURVEY PERFORMED FEBRUARY 12-20, 2019 BY RENT GROUND ELEVATIONS MAY VARY FROM THOSE SHOWN DUE TO SITE WORK THAT HAS BEEN SURVEY WAS PERFORMED. D ALL VERIFY EXISTING CONTOURS PRIOR TO THE START OF WORK. ANY ADDITIONAL PAYMENT OR EXTENSION OF CONTRACT TIME FOR WORKING WITH SATURATED SOILS OR PAGE DUE TO RAINFALL, RUNOFF AND INFILTRATION. ALL TAKE ALL NECESSARY PRECAUTIONS TO PROTECT EXISTING ROADS, BENCHMARKS AND EXISTING OR WELLS DURING THE CONSTRUCTION PERIOD. THE CONTRACTOR SHALL BE SOLEY RESPONSIBLE FOR ANY HICH MIGHT BE INCURRED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PROTECT THE OR WELLS, BENCHMARKS AND EXISTING ROADS. (ISTING UNDERGROUND UTILITIES HAVE NOT BEEN ESTABLISHED BY THE OWNER OR ENGINEER. THE ETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO E FOR ANY AND ALL DAMAGES WHICH MIGHT BE OCCASIONED BY THE CONTRACTORS FAILURE TO EXACTLY E ANY AND ALL UTILITIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING PROPER SAFE ROM ALL UTILITY EASEMENTS OR LINES. STING" IS NOT PERMITTED ON THIS PROJECT. EVATIONS SHALL MATCH EXISTING GROUND ELEVATIONS EXCEPT AS SHOWN ON THE PLANS. ALL EXCESS AVATION AND GRADING SHALL BE PLACED IN DESIGNATED STOCKPILE LOCATIONS AS APPROVED BY THE ENCOUNTERED DURING EXCAVATION, THE OWNER SHALL BE NOTIFIED AND THE WASTE REMOVED AND ESIGNATED AS APPROVED BY THE OWNER. TRANSPORT OF SOIL TO FILL AREAS SHALL BE CONDUCTED BY NO ADDITIONAL EXPENSE TO THE OWNER. ALL CONSTRUCT, AND UPON COMPLETION OF THE PROJECT, REMOVE TEMPORARY CONSTRUCTION ACCESS SHALL BE LOCATED AS APPROVED BY THE OWNER. DRAINAGE PATTERNS AT THE SITE SHALL NOT BE INSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONSTRUCTION AND MAINTENANCE OF STRUCTURES, INCLUDING CULVERTS, AT NO ADDITIONAL COST TO THE OWNER. LL INSTALL, MAINTAIN, AND UPON COMPLETION OF THE PROJECT, REMOVE TEMPORARY EROSION AND AS APPROVED BY GCERG AND IN ACCORDANCE WITH THE SITE SWPPP AND PURSUANT TO TPDES CONTROLS SHALL BE PLACED AT THE LIMITS OF DISTURBED AREAS AND AT INTERMEDIATE LOCATIONS FLOW IS LIKELY. CTION SLOPES SHALL NOT BE GREATER THAN 2H:1V. STEEPER SLOPES WILL ONLY BE ALLOWED IF THE A GEOTECHNICAL ENGINEERING REPORT SPECIFYING MAXIMUM SLOPES AND THE DURATION FOR WHICH REMAIN IN PLACE. ALL REMOVE ALL VEGETATION WITHIN THE CONSTRUCTION LIMITS AS REQUIRED TO CONSTRUCT THE PROJECT. . BE REMOVED BY CONTRACTOR AT NO ADDITIONAL EXPENSE TO OWNER. LL IMMEDIATELY REPORT TO THE ENGINEER ANY ERROR OR DISCREPANCY FOUND ONCE THE CONTRACT LLY REVIEWED AND ALL ASPECTS OF FIELD WORK HAVE BEEN VERIFIED. IN THE EVENT THE CONTRACTOR ON AN ITEM WHERE AN ERROR EXISTS, IT SHALL BE DEEMED THAT THE CONTRACTOR BID AND INTENDED STRINGENT OR HIGHER QUALITY REQUIREMENT WITHOUT AN INCREASE IN CONTRACT SUM OR TIME. THE LSO BE RESPONSIBLE TO CORRECT ANY FAILURE OF COMPANY PARTS TO COORDINATE OR FIT PROPERLY AS A RESULT OF CONTRACTOR FAILURE TO RAISE OR RESOLVE A DISCREPANCY. PECIFICATIONS SHOULD AGREE WITH EACH OTHER, AND WORK CALLED FOR BY DRAWINGS AND NOT CATION, OR VICE VERSA, SHALL BE FURNISHED BY BOTH. WHEN DISCREPANCIES EXIST BETWEEN SCALE AND NSIONÉD FIGURE SHALL BE USED. CH SUBCONTRACTOR SHALL VERIFY ALL GRADES, LINES, LEVELS, AND DIMENSIONS AS INDICATED ON HALL REPORT ERRORS TO THE ENGINEER BEFORE COMMENCING WORK. THE CONTRACTOR SHALL ESTABLISH EAST TWO WIDELY SEPARATED PLACES, AND AS WORK PROGRESSES THE CONTRACTOR WILL MAINTAIN AND VERTICAL CONTROL. PROVIDE EROSION CONTROL BY SEEDING FOR ALL AREAS DISTURBED BY CONTRACTOR DURING THE IS PROJECT. THE CONTRACTOR SHALL NOT DISTURB ANY AREA WITHOUT THE APPROVAL OF THE ENGINEER. SEEDING SHALL CONFORM TO STANDARD SPECIFICATION 329200. L BE PERMITTED TO BE SPILLED FROM THE HAUL TRUCKS. ANY CCR MATERIAL SPILLED ON THE HAUL TELY BE CONTAINED AND REMOVED. THE CONTRACTOR SHALL FOLLOW CHARAH'S CCR SPILL RESPONSE ANY SPILL WITH CHARAH/GCERG AS REQUIRED. IWATER THAT HAS COME INTO CONTACT WITH CCR MATERIAL IS TO BE CONSIDERED CONTACT WATER. TROL THE WATER ON SITE IN COMPLIANCE WITH THE TPDES PERMIT AND THE PROJECT WATER HE LATEST EDITION. RATION OF H2S POISONOUS GAS MAY BE PRESENT NEAR DISCHARGE DRAINS, LEACHATE EQUIPMENT OR DETECTION EQUIPMENT IS REQUIRED WHEN WORKING IN AREAS WHERE H2S MAY BE PRESENT. HATE WATER MAY BE ACIDIC. CONTRACTOR TO TAKE ANY NECESSARY PRECAUTIONS WHILE WORKING WITH RMINE, INSTALL AND MAINTAIN APPROPRIATE STORMWATER POLLUTION PREVENTION BMP'S IN ACCORDANCE R POLLUTION PREVENTION PLAN AND AS DIRECTED BY THE OWNER. CONTRACTOR WILL BE RESPONSIBLE PECTIONS AND DOCUMENTATION REQUIRED UNDER THE SITE'S STORMWATER POLLUTION PLAN. IRE NOI FOR TXR150000 CONSTRUCTION TPDES PERMIT COVERAGE AND POST THE SITE NOTICE AT THE SITE 244. NOI MUST BE SUBMITTED A MINIMUM OF 7 DAYS PRIOR TO THE START OF CONSTRUCTION. 35 26.17 FOR MINIMUM SOIL COVER REQUIREMENTS FOR VEHICLE USE ON TOP OF GEOMEMBRANES. Α

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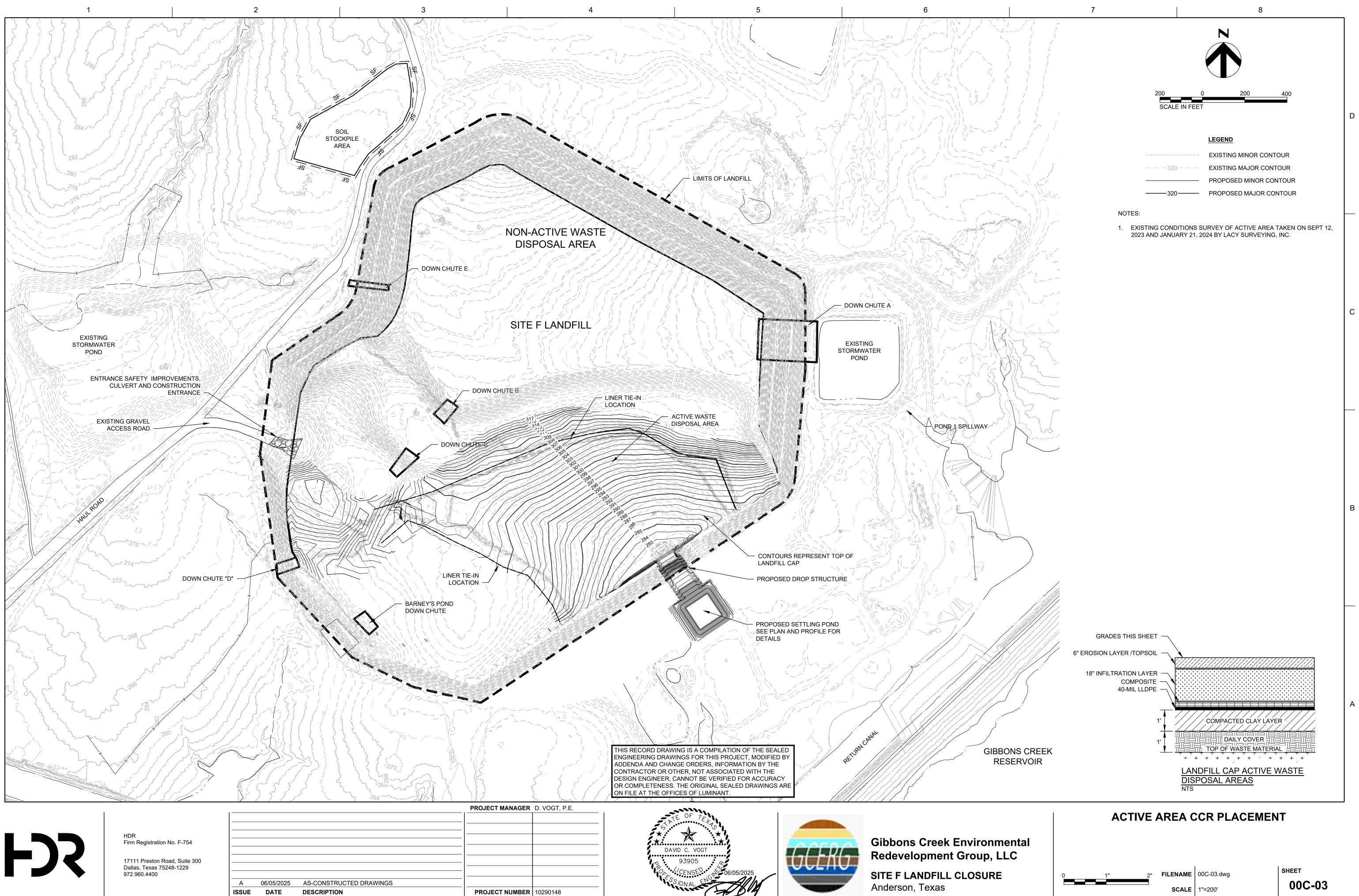
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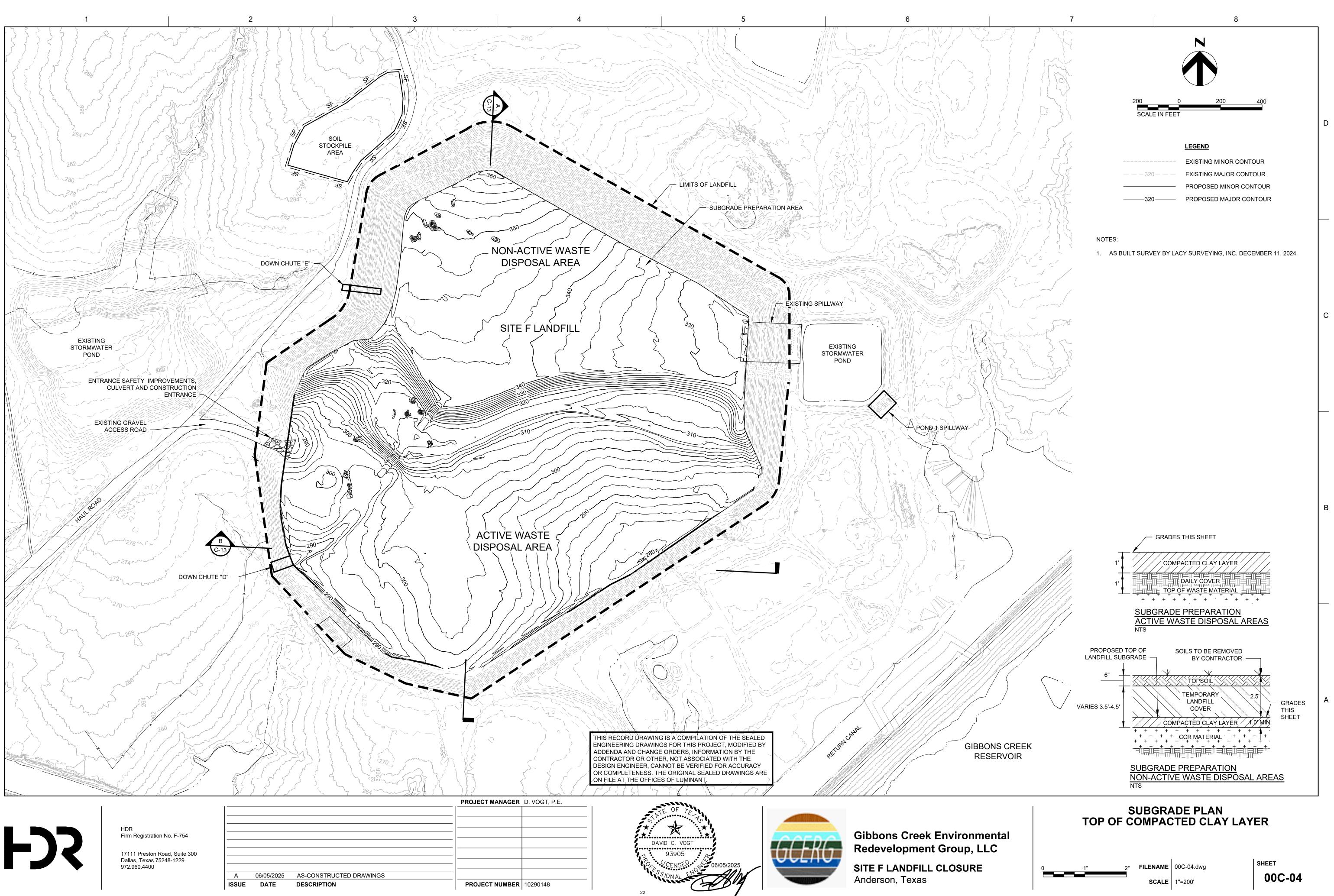
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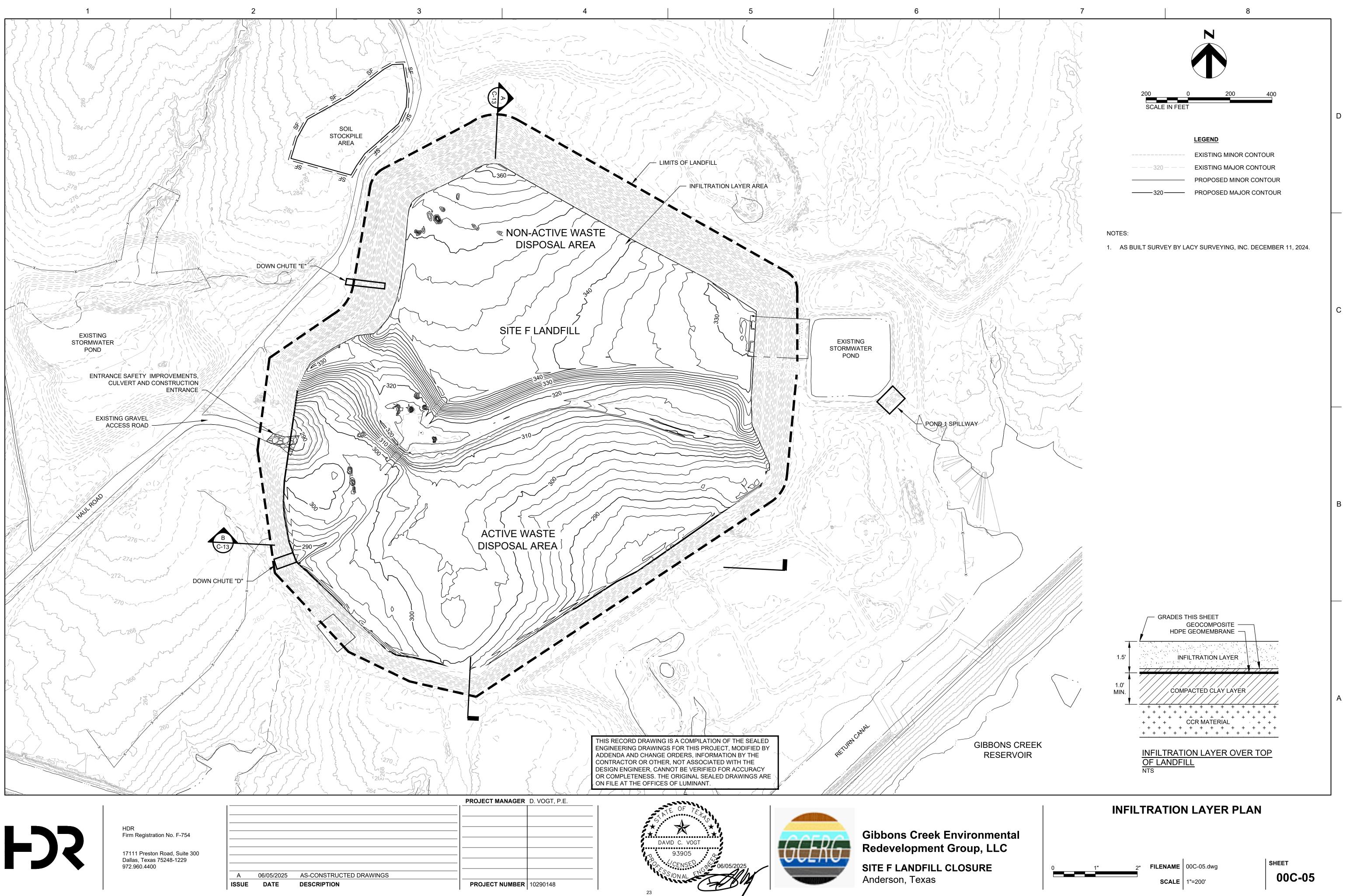
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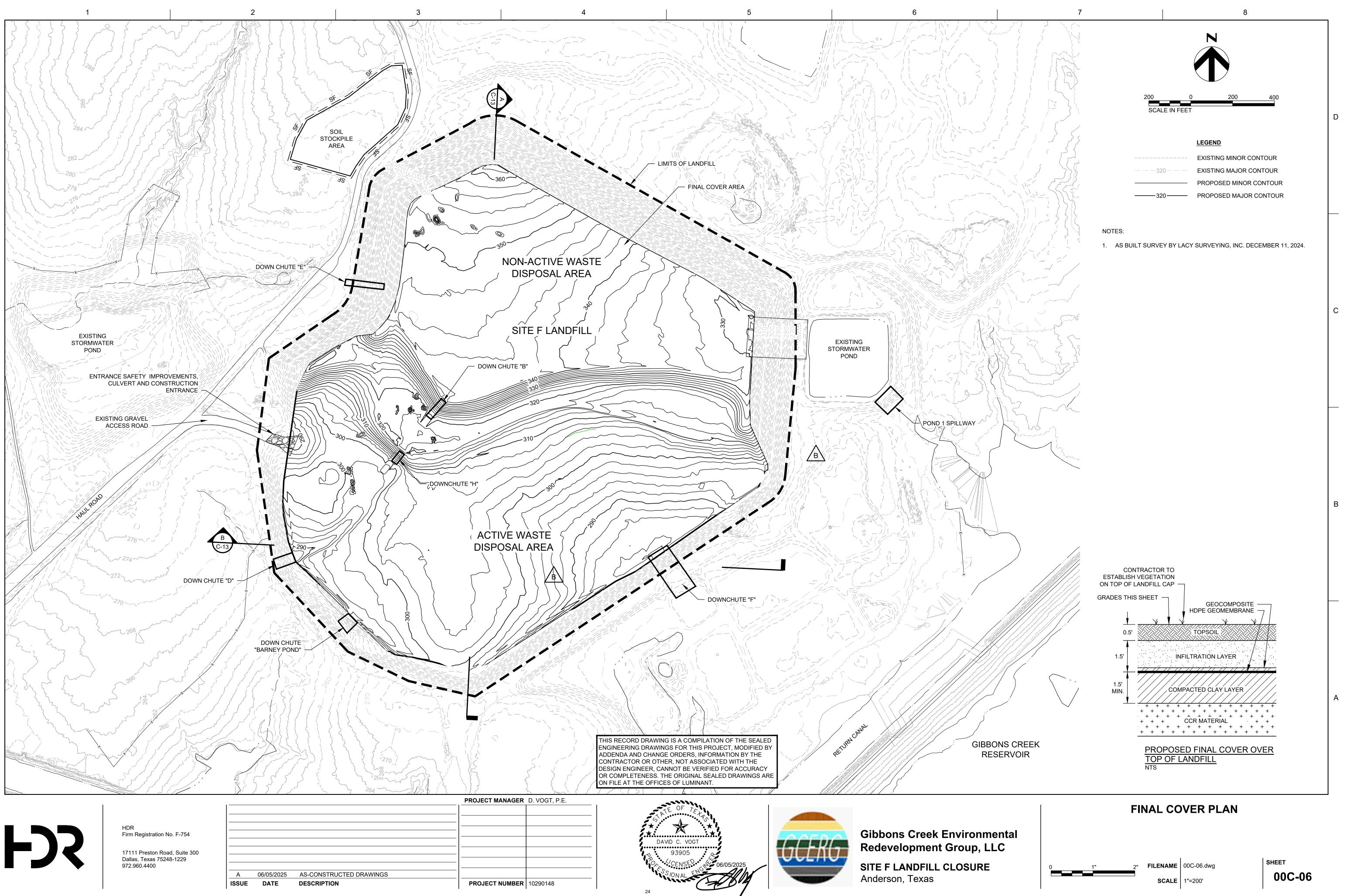


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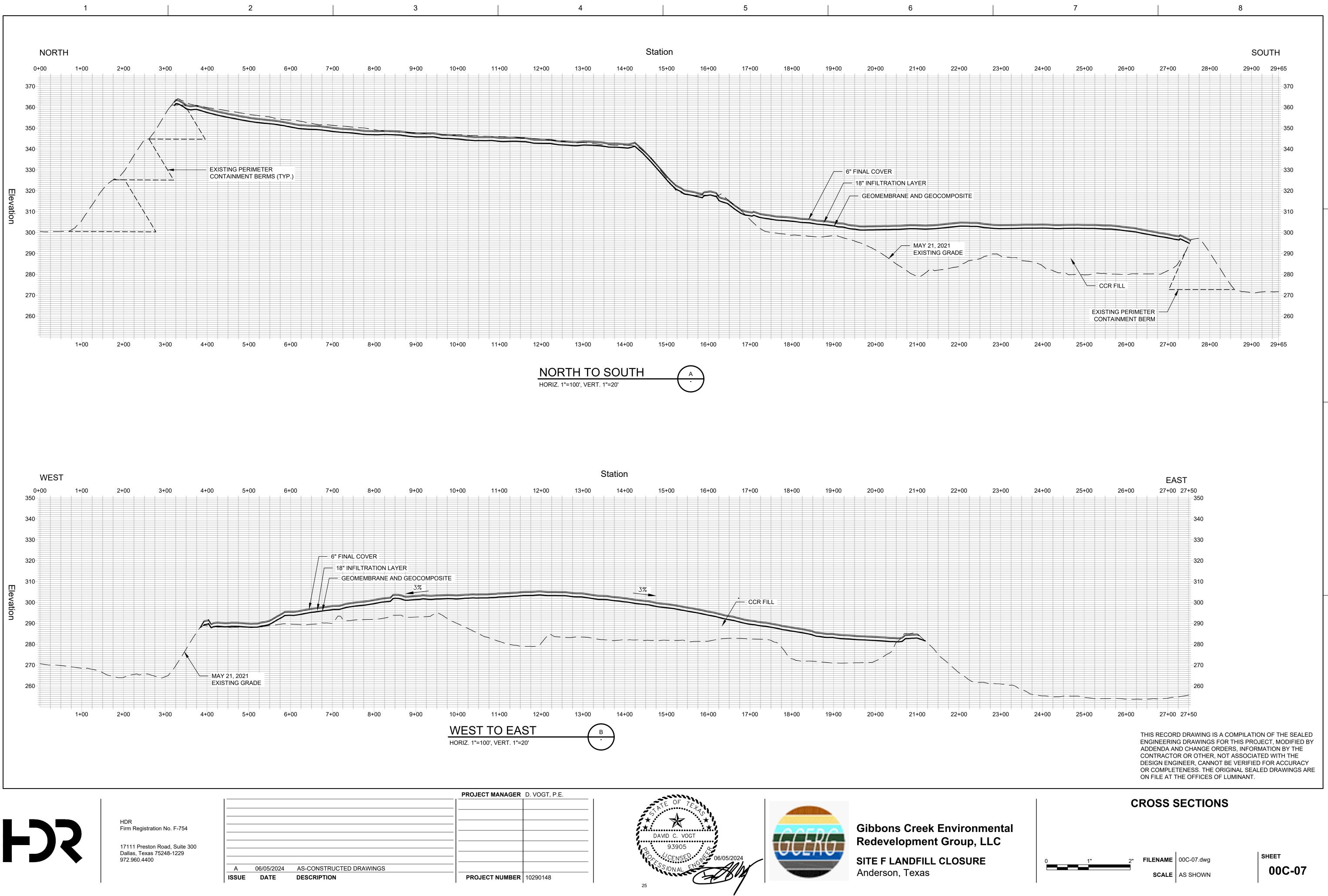




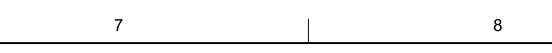
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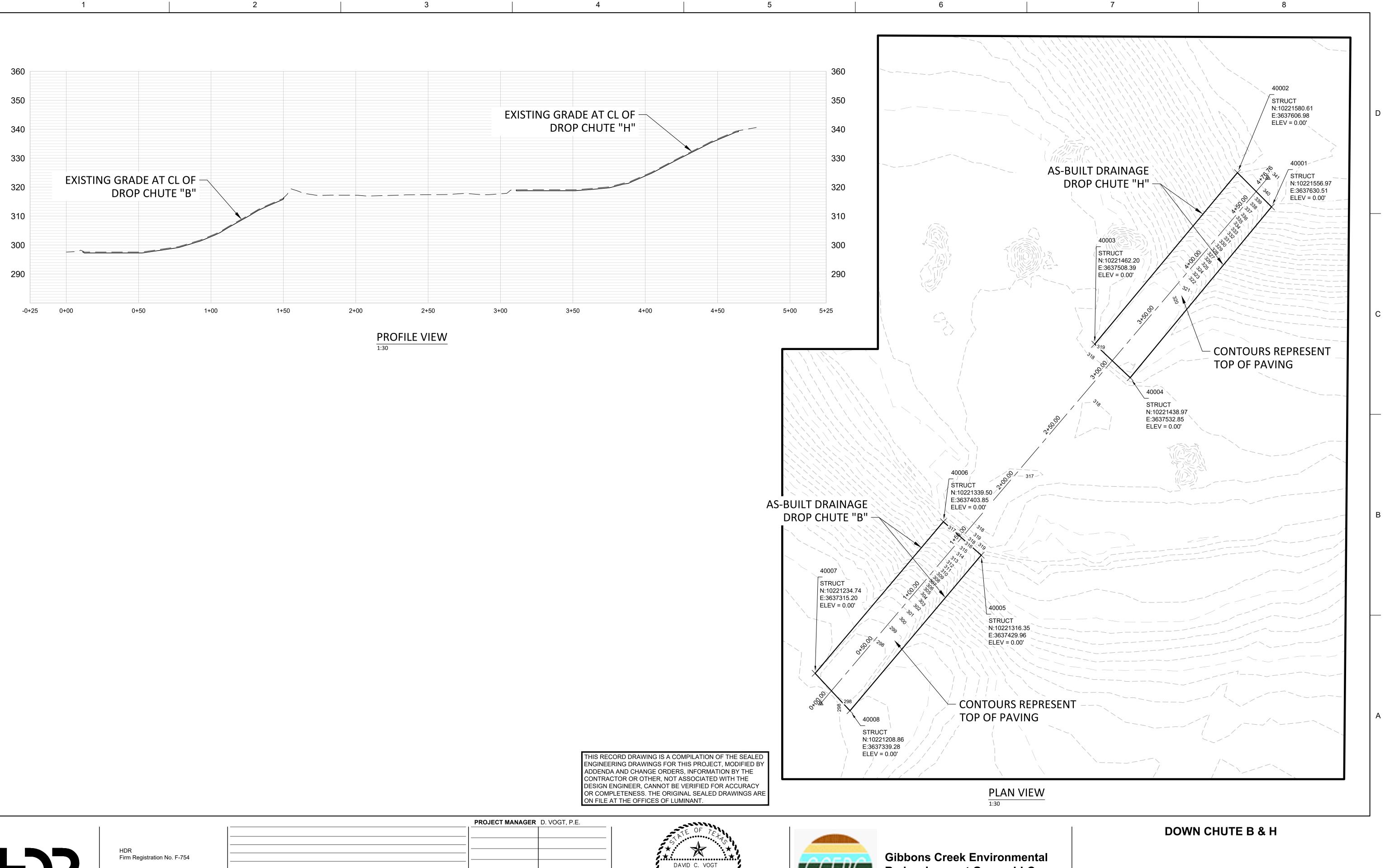


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PROJECT MANAGER	D. VOGT, P.E.
PROJECT NUMBER	10290148



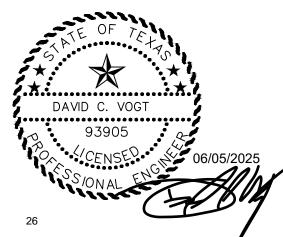


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A	06/05/2025
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PROJECT NUMBER	10290148

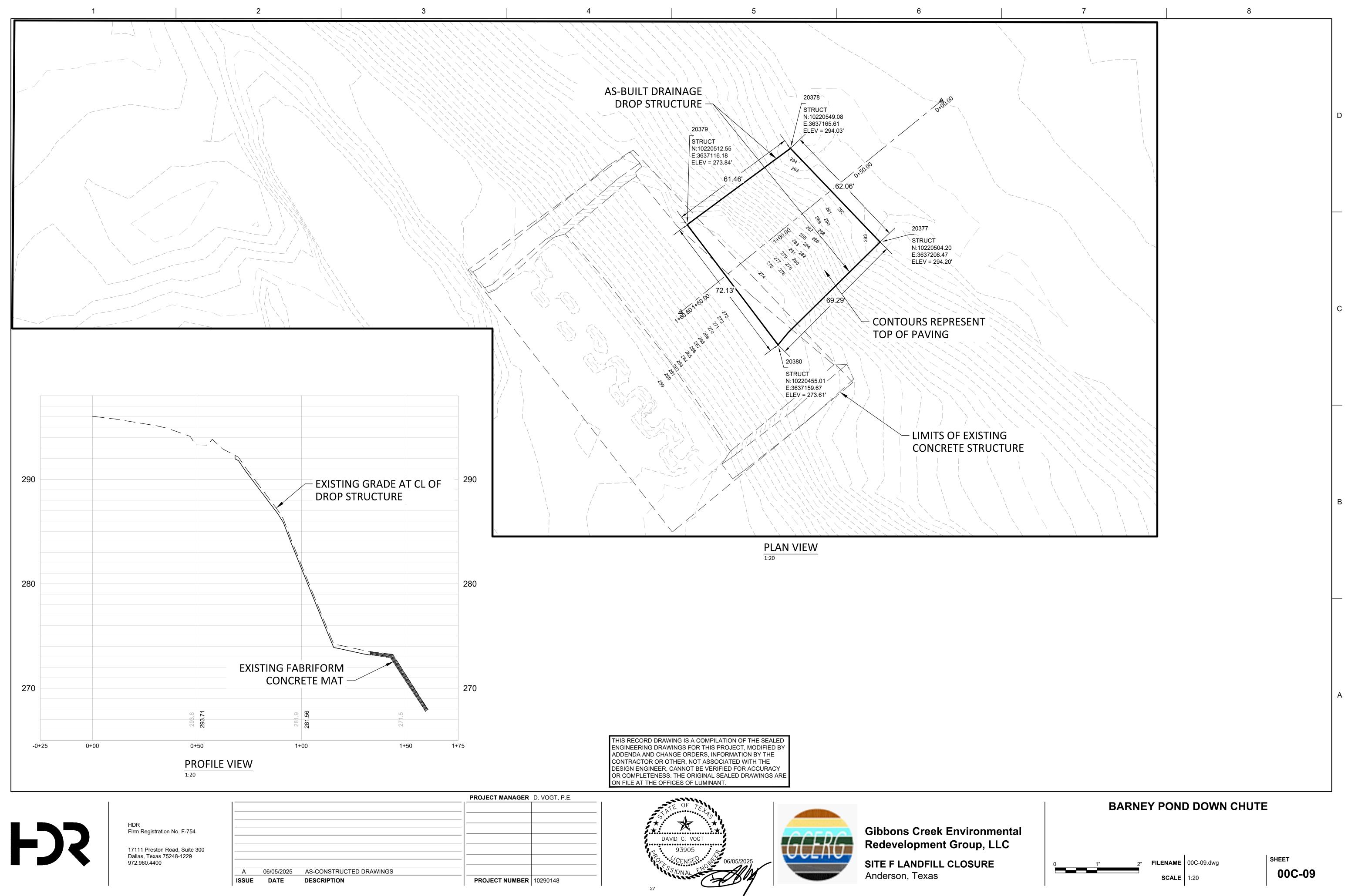




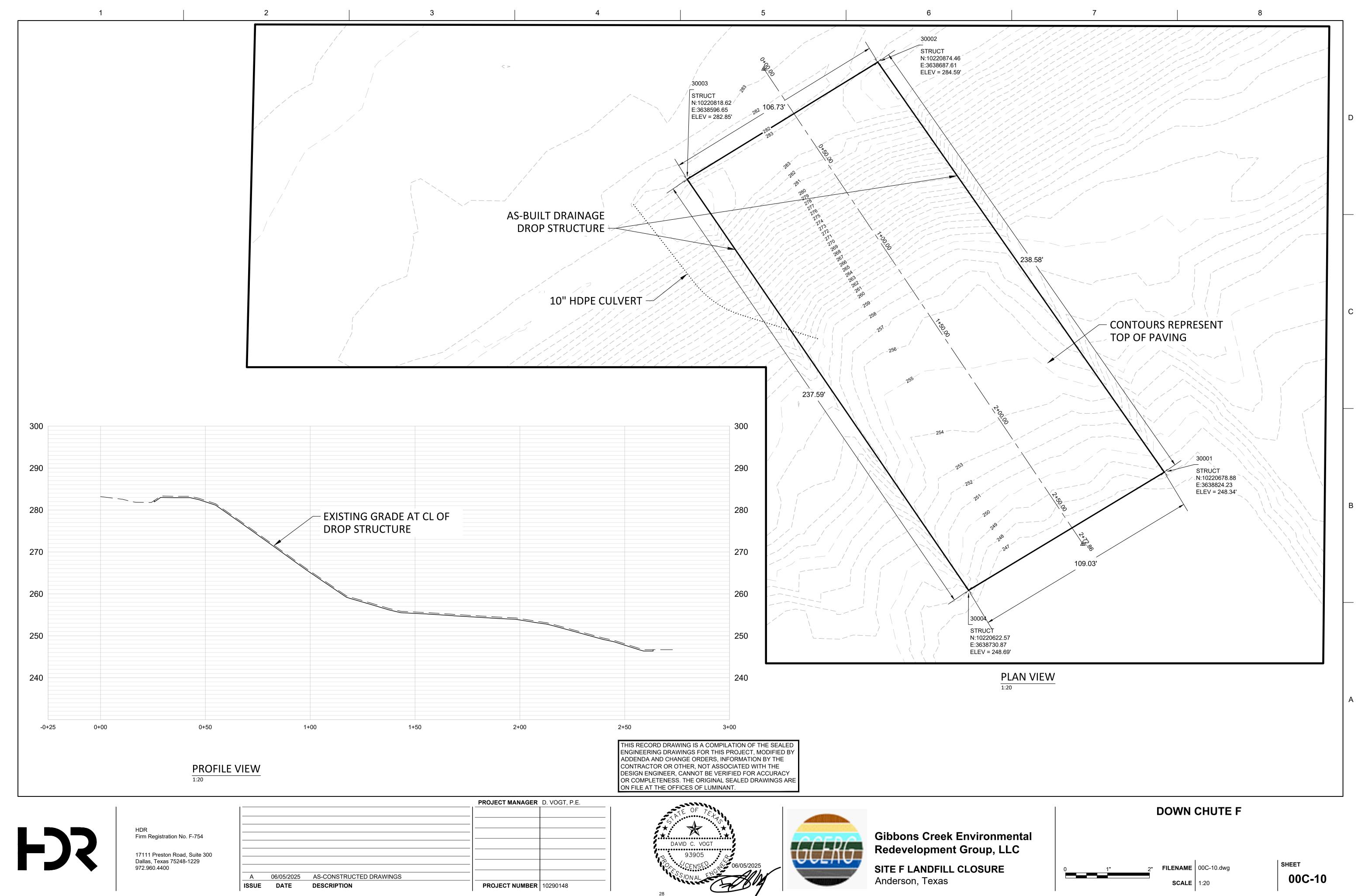
Redevelopment Group, LLC

SITE F LANDFILL CLOSURE Anderson, Texas

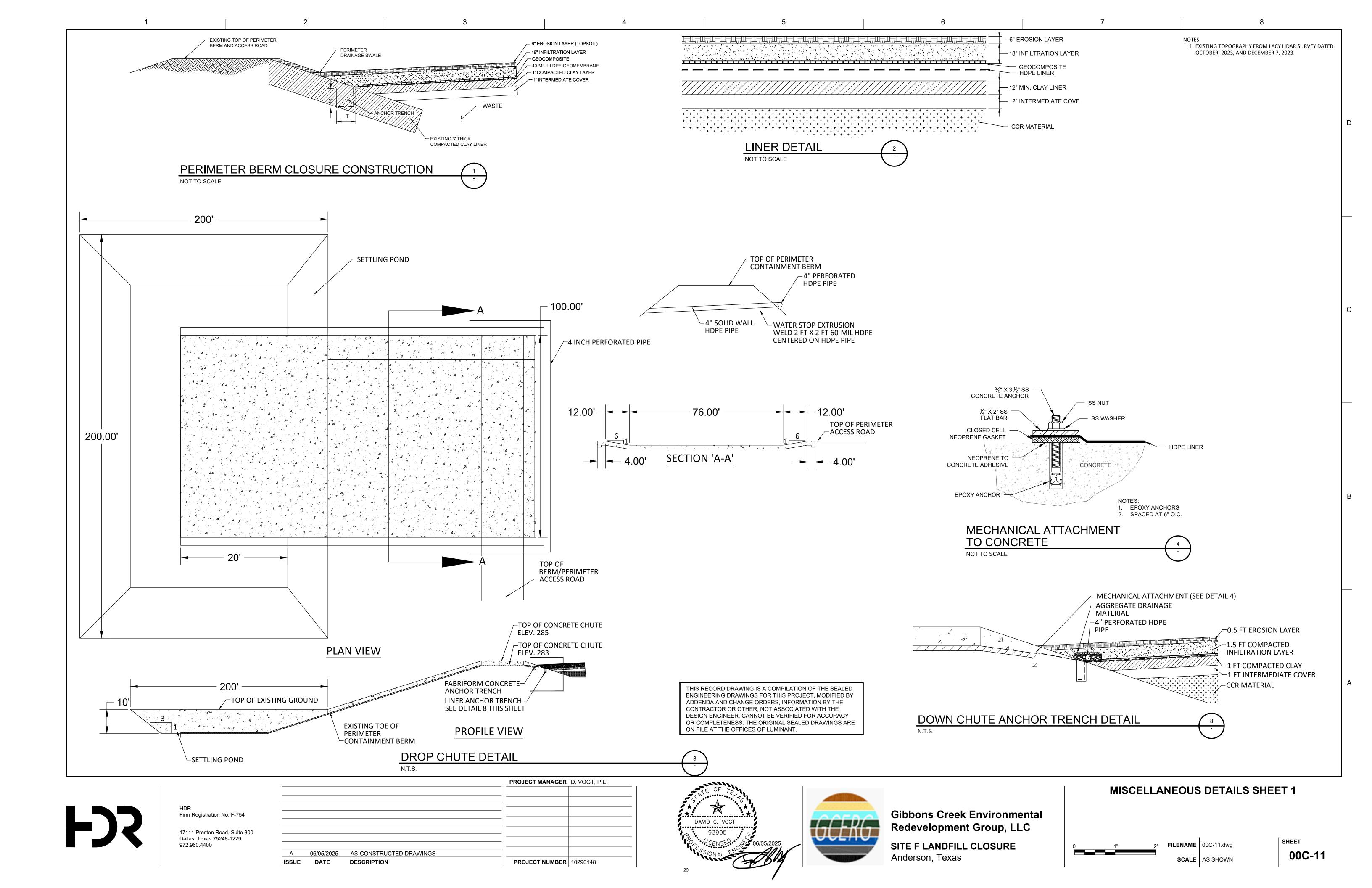
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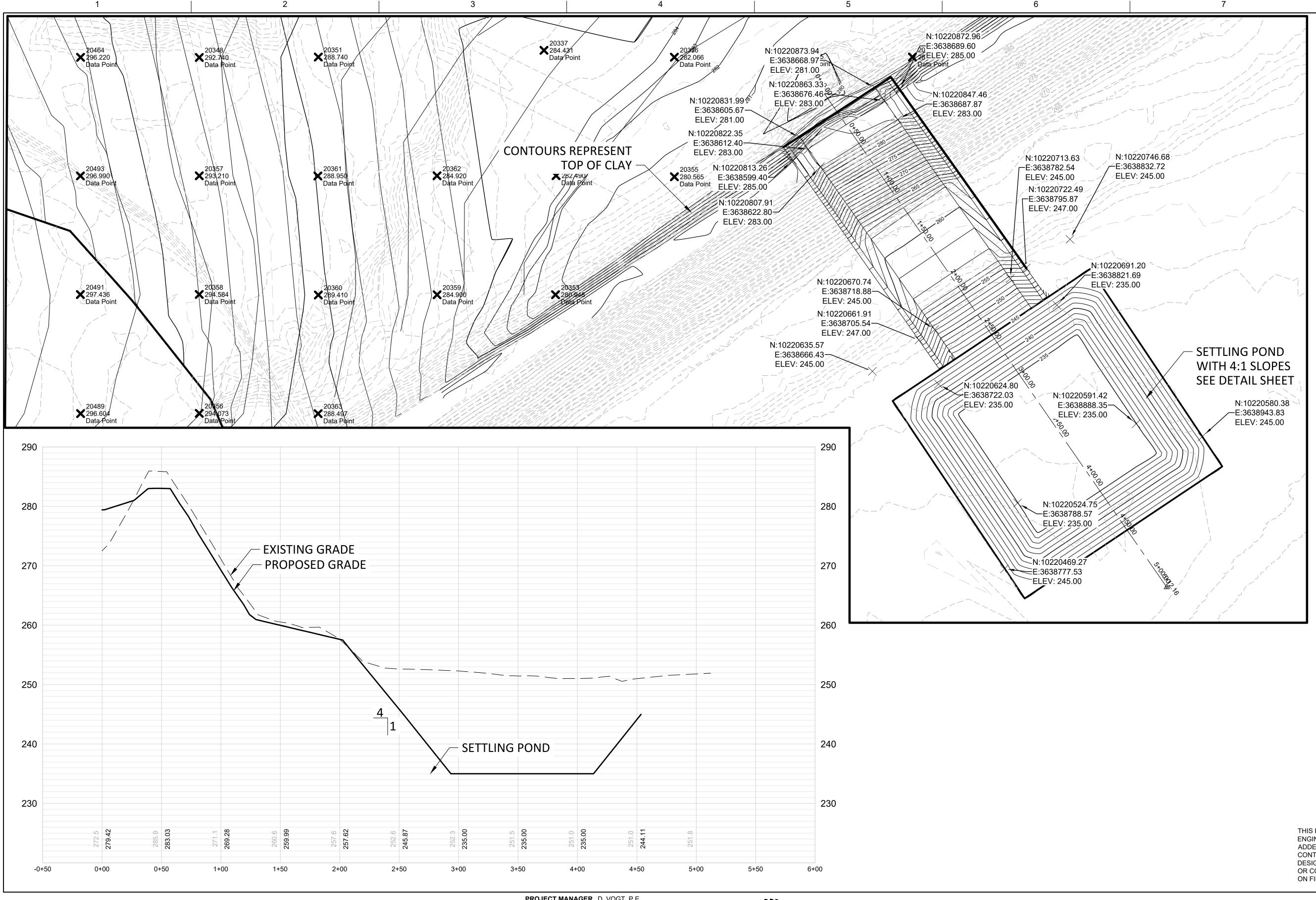


PROJECT MANAGER	D. VOGT, P.E.
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PROJECT NUMBER	10290148
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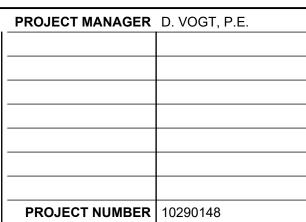


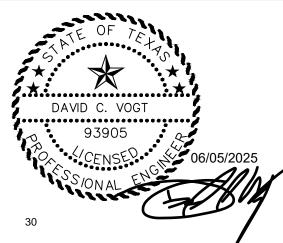
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HDR Firm Registration No. F-754

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MISCELLANEOUS DETAILS SHEET 2

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APPENDIX B

LANDFILL CAP MANUFACTURER QUALITY CONTROL CERTIFICATES